Conclusion

Nuclear Installation Lifecycle: Modeling and Simulation of Design Basis and Beyond Design Basis ESSI Behavior

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Outline

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Modeling and Simulation of ESSI for Nuclear Installations

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Motivation

Improve modeling and simulation for infrastructure objects

Expert numerical modeling and simulation tool

Control and reduce modeling uncertainty

Goal: Predict and Inform rather than fit

Engineer needs to know!

System for modeling and simulation of Earthquakes and/or Soils and/or Structures and their Interaction: Real-ESSI, http://real-essi.info/



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Prediction under Uncertainty

► Modeling Uncertainty, Simplifying assumptions

Low, medium, high sophistication modeling and simulation Choice of sophistication level for confidence in results

► Parametric Uncertainty, $M\ddot{u}_i + C\dot{u}_i + K^{ep}u_i = F(t)$,

Uncertain mass *M*, viscous damping *C* and stiffness K^{ep} Propagation of uncertainty in loads, F(t)Results are PDFs and CDFs for σ_{ij} , ϵ_{ij} , u_i , \dot{u}_i , \ddot{u}_i



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Modeling Uncertainty

- Important (?!) features are simplified, 1C vs 3C, inelasticity
- Modeling simplifications are justifiable if one or two level higher sophistication model demonstrates that features being simplified out are not important



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Parametric Uncertainty: Soil Stiffness and Strength



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Regional Geophysical Models

- ► Free Field seismic motions on regional scale
- ► Knowledge of geology (deep and shallow) needed
- Developed using SW4 and/or Real-ESSI
- Collaboration with LLNL: Dr. Rodgers, Dr. Pitarka and Dr. Petersson



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Regional Geophysical Models



Rodgers and Pitarka

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Regional Geophysical Models



USGS

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Example Regional Model (Rodgers)





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Energy Input and Dissipation

Energy input, dynamic forcing

Energy dissipation outside SSI domain:

SSI system oscillation radiation Reflected wave radiation

Energy dissipation/conversion inside SSI domain:

Inelasticity of soil, contact zone, structure, foundation, dissipators

Viscous coupling with internal/pore fluids, and external fluids

Numerical energy dissipation/production



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Plastic Energy Dissipation

Single elastic-plastic element under cyclic shear loading

Difference between plastic work and plastic dissipation Plastic work can decrease

Plastic dissipation always increases



Energy Dissipation Control



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Inelastic Modeling of Soil Structure Systems

► Soil, inelastic, elastic-plastic

Dry, single phase Unsaturated, partially saturated Fully saturated

Contact, inelastic, soil/rock – foundation

Dry, single phase,

Normal, hard and soft, gap open/close Friction, nonlinear

Fully saturated, suction, excess pressure, buoyant force

Structure, inelastic, damage, cracks

Nonlinear/inelastic 1D reinforced concrete fiber beam Nonlinear/inelastic 3D reinforced concrete solid element Alcali Silica Reaction concrete modeling



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Inelastic Soil and Inelastic Contact

- Shear velocity of soil $V_s = 500 m/s$
- Undrained shear strength (Dickenson 1994) $V_s[m/s] = 23(S_u[kPa])^{0.475}$
- For $V_s = 500 m/s$ Undrained Strength $S_u = 650 kPa$ and Young's Modulus of E = 1.3 GPa
- ► von Mises, Armstrong Frederick kinematic hardening $(S_u = 650 kPa \text{ at } \gamma = 0.01\%; h_a = 30 MPa, c_r = 25)$
- Soft contact (concrete-soil), gaping and nonlinear shear



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Acceleration Traces, Elastic vs Inelastic





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Displacement Traces, Elastic vs Inelastic





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Energy Dissipation in a Large-Scale Model



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Uncertainty Propagation through Inelastic System

Incremental el–pl constitutive equation

$$\Delta \sigma_{ij} = \mathcal{E}_{ijkl}^{\mathcal{EP}} \Delta \epsilon_{kl} = \left[\mathcal{E}_{ijkl}^{\mathcal{el}} - \frac{\mathcal{E}_{ijmn}^{\mathcal{el}} m_{mn} n_{pq} \mathcal{E}_{pqkl}^{\mathcal{el}}}{n_{rs} \mathcal{E}_{rstu}^{\mathcal{el}} m_{tu} - \xi_* h_*} \right] \Delta \epsilon_{kl}$$

Dynamic Finite Elements

$$M\ddot{u}_i + C\dot{u}_i + K^{ep}u_i = F(t)$$





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Probabilistic Elastic-Plastic Modeling



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Stochastic Elastic-Plastic Finite Element Method

- Material uncertainty expanded into stochastic shape funcs.
- ► Loading uncertainty expanded into stochastic shape funcs.
- Displacement expanded into stochastic shape funcs.

$$\begin{bmatrix} \sum_{k=0}^{P_{d}} < \Phi_{k} \Psi_{0} \Psi_{0} > K^{(k)} & \dots & \sum_{k=0}^{P_{d}} < \Phi_{k} \Psi_{P} \Psi_{0} > K^{(k)} \\ \sum_{k=0}^{F_{d}} < \Phi_{k} \Psi_{0} \Psi_{1} > K^{(k)} & \dots & \sum_{k=0}^{P_{d}} < \Phi_{k} \Psi_{P} \Psi_{1} > K^{(k)} \\ \vdots \\ \sum_{k=0}^{P_{d}} < \Phi_{k} \Psi_{0} \Psi_{P} > K^{(k)} & \dots & \sum_{k=0}^{M} < \Phi_{k} \Psi_{P} \Psi_{P} > K^{(k)} \end{bmatrix} \begin{bmatrix} \Delta u_{10} \\ \vdots \\ \Delta u_{N0} \\ \vdots \\ \Delta u_{1P_{u}} \\ \vdots \\ \Delta u_{NP_{u}} \end{bmatrix} = \begin{bmatrix} \sum_{i=0}^{P_{f}} f_{i} < \Psi_{0} \zeta_{i} > \\ \sum_{i=0}^{T_{f}} f_{i} < \Psi_{2} \zeta_{i} > \\ \vdots \\ \sum_{i=0}^{P_{f}} f_{i} < \Psi_{2} \zeta_{i} > \\ \vdots \\ \Delta u_{NP_{u}} \end{bmatrix}$$



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SEPFEM: System Size

- SEPFEM offers a complete solution (single step)
- It is NOT based on Monte Carlo approach
- System of equations does grow (!)

# KL terms material	# KL terms load	PC order displacement	Total # terms per DoF
4	4	10	43,758
4	4	20	3,108,105
4	4	30	48,903,492
6	6	10	646,646
6	6	20	225,792,840



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SEPFEM: Example in 1D



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Summary

- Numerical modeling to predict and inform, rather than fit
- Engineer needs to know
- Model, simulate and understand full life cycle of an object
- Funding from and collaboration with the US-DOE, US-NRC, US-NSF, US-BR, US-FEMA CNSC-CCSN, UN-IAEA, and Shimizu Corp. is greatly appreciated,
- More info: http://real-essi.info/



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