

# Full Seismic Wave Inversion in 3D for ESSI Analysis

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# Outline

Introduction

Inverse Wave Field Analysis

Summary

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# Motivation

Improve modeling and simulation of nuclear installations

Reduction of modeling uncertainty

Development of full 3D/3C wave fields for ESSI analysis

Use surface, structure and limited downhole motion measurements for development of wave fields

# Dedication

Robert P. Kennedy, 1939-2018



"Response of a soil structure system is nonlinear, and I would really like to know what that response is!"

Nebojša Orbović, 1962-2021



"As an engineer, I have to know what are response sensitivities to modeling choices and model parameters."

# Prediction under Uncertainty

- Modeling Uncertainty, Simplifying assumptions

  - Low, medium, high sophistication modeling and simulation

  - Choice of sophistication level for confidence in results

- Parametric Uncertainty,  $M\ddot{u}_i + C\dot{u}_i + K^{ep}u_i = F(t)$ ,

  - Uncertain mass  $M$ , viscous damping  $C$  and stiffness  $K^{ep}$

  - Propagation of uncertainty in loads,  $F(t)$

  - Results are PDFs and CDFs for  $\sigma_{ij}$ ,  $\epsilon_{ij}$ ,  $u_i$ ,  $\dot{u}_i$ ,  $\ddot{u}_i$

# Goal: Reduction of Modeling Uncertainty

- Modeling Uncertainty: introduced with unnecessary and unrealistic modeling simplification
- Simplified (or inadequate/wrong) modeling: important features are missed (3C (6C) seismic ground motions, inelasticity, etc.)
- Modeling simplifications are justifiable if one, two or higher level sophistication model demonstrates that features being simplified out are not important
- Use of HPC for low modeling uncertainty and direct probabilistic modeling and simulations

# Outline

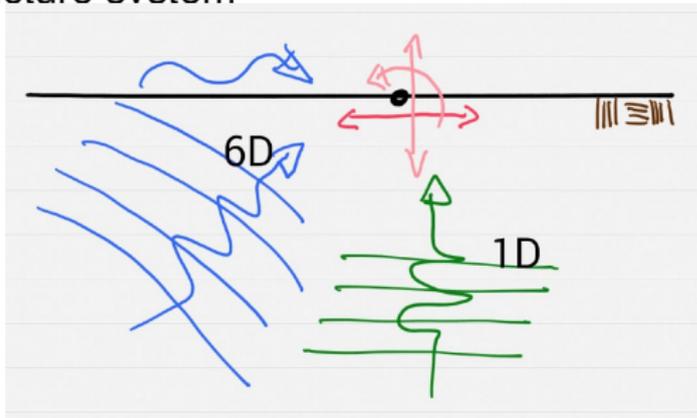
Introduction

**Inverse Wave Field Analysis**

Summary

## ESSI: 6C or 1C Seismic Motions

- ▶ Assume that a full 6C (3C) motions at the surface are only recorded in one horizontal direction
- ▶ From such recorded motions one can develop a vertically propagating shear wave (1C) in 1D
- ▶ Apply such vertically propagating shear wave to same soil-structure system

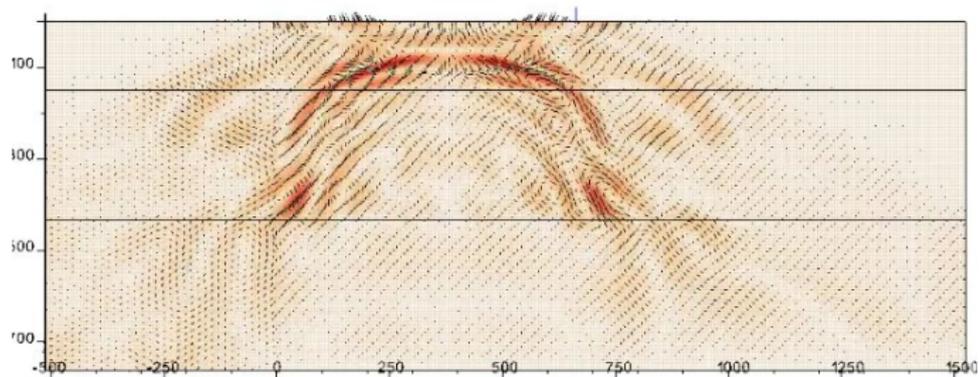
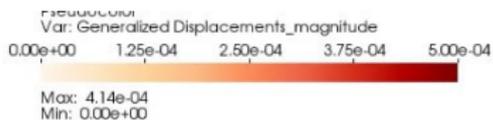


# Realistic Ground Motions

## ► Free field seismic motion models

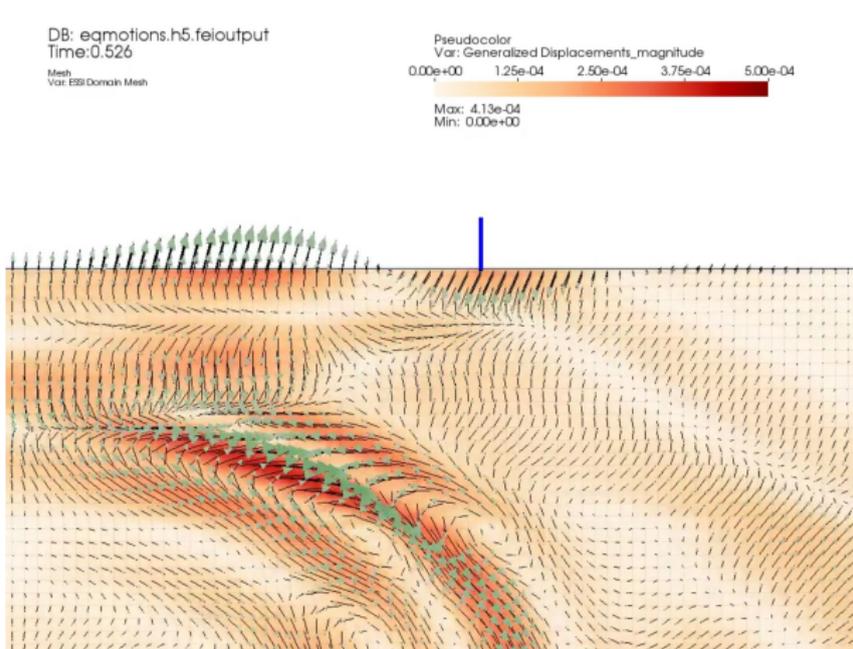
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Domain Mesh



# Development of Realistic Motions

- Sources will send both P and S waves



# 1C vs 6C Free Field Motions

- ▶ One component of motions, 1C from 6C
- ▶ Excellent fit

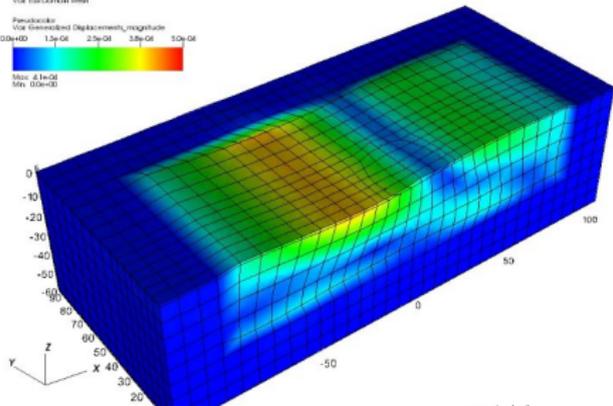
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Vol: 858 Domain Mesh

Paraview Color  
Var: Generalized Displacements\_magnitude

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Max: 4.1e-04  
Min: 0.0e+00



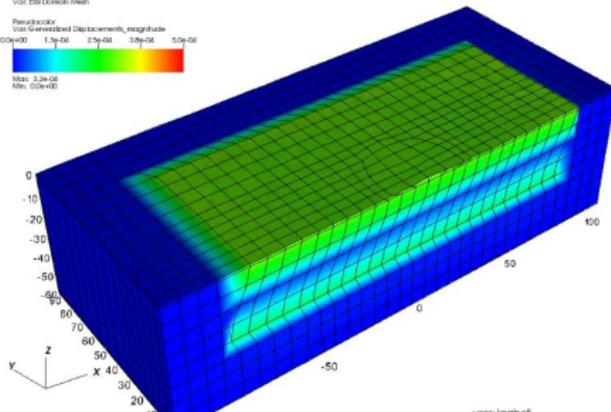
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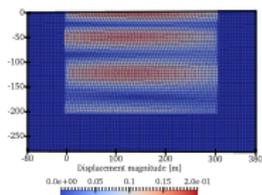
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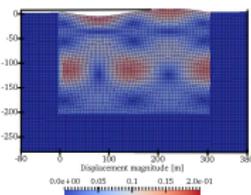
(MP4) (MP4)

# 1C vs 6C Free Field Motions



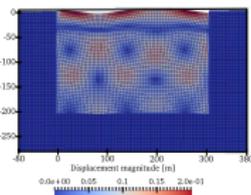
(a)

$$f = 5\text{Hz } \theta = 10^\circ$$



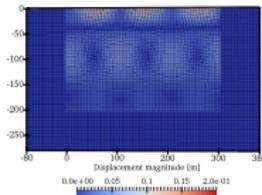
(b)

$$f = 5\text{Hz } \theta = 45^\circ$$



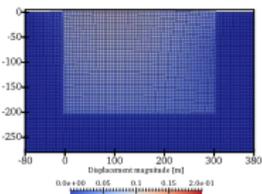
(c)

$$f = 5\text{Hz } \theta = 60^\circ$$



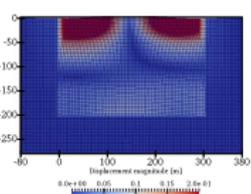
(d)

$$f = 5\text{Hz } \theta = 80^\circ$$



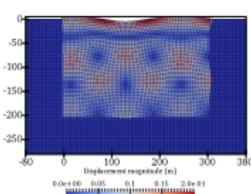
(e)

$$f = 1\text{Hz } \theta = 60^\circ$$



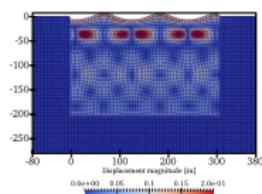
(f)

$$f = 2.5\text{Hz } \theta = 60^\circ$$



(g)

$$f = 5\text{Hz } \theta = 60^\circ$$

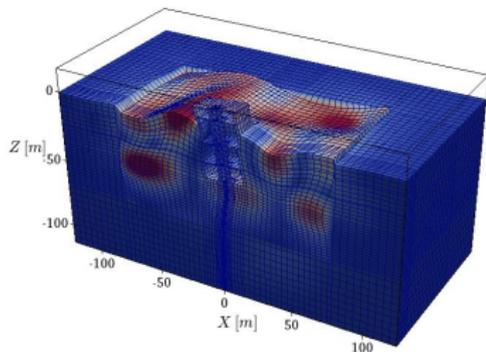


(h)

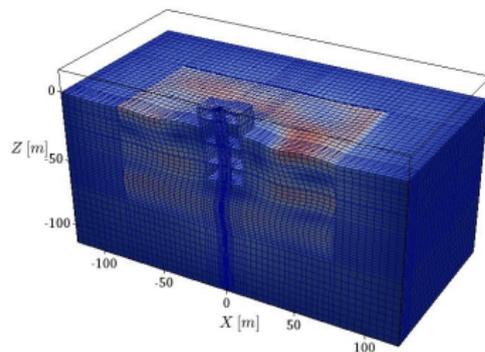
$$f = 10\text{Hz } \theta = 60^\circ$$

# SMR ESSI, 3C vs 3×1C

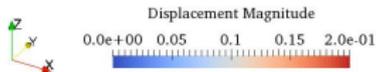
3C



3 × 1C



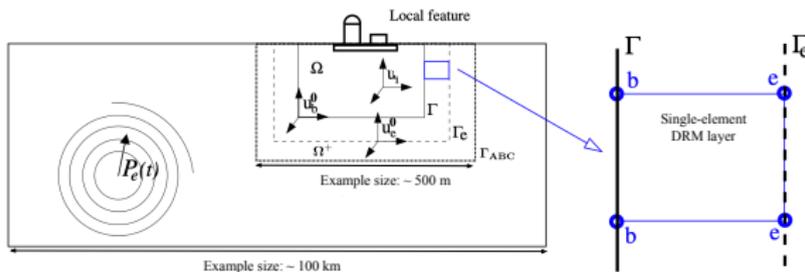
(OGV)



# Development of 3D/3C Wave Fields

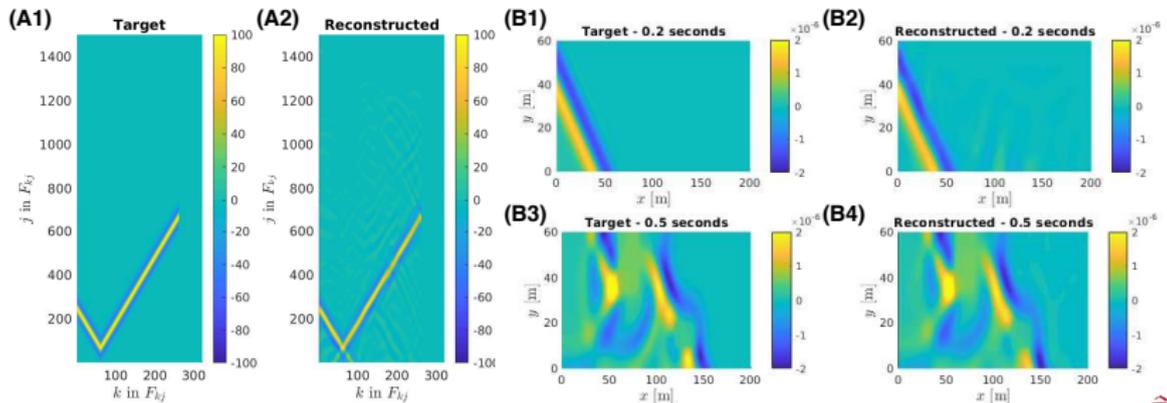
- PDE-constrained optimization
- Evaluate gradient of a misfit between measured and computed wave fields
- Optimize DRM effective forces

$$\mathbf{P}_{eff} = \begin{bmatrix} 0 \\ -\mathbf{M}_{be}^{\Omega^+} \ddot{\mathbf{u}}_e^0 - \mathbf{K}_{be}^{\Omega^+} \mathbf{u}_e^0 \\ +\mathbf{M}_{eb}^{\Omega^+} \ddot{\mathbf{u}}_b^0 + \mathbf{K}_{eb}^{\Omega^+} \mathbf{u}_b^0 \end{bmatrix}$$



# Development of 3D/3C Wave Fields

- Preliminary results encouraging
- Minimizing number of measuring points
- Measurements of 1C, 2C or 3C motions
- Recreate full 3D/3C wave field



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- Importance of using realistic 3D/3C seismic wave fields
- PDE-constrained optimization
- Develop optimized DRM effective forces
- Use surface and at depth measurements (1C, 2C, 3C)
- Develop full, 3C wave field
- `http://real-essi.us`