

Stochastic Elastic-Plastic Finite Element Method

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Outline

Motivation

Motivation and Overview

SEPFEM

Probabilistic Elasto–Plasticity

SEPFEM Formulations

An Application

Seismic Wave Propagation Through Uncertain Soils

Summary

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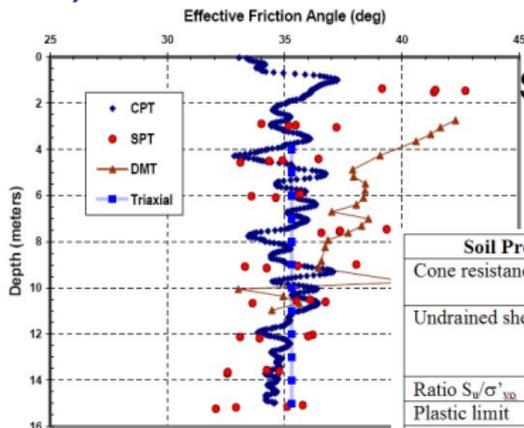
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(Geo-) Materials are Inherently Uncertain



Spatial Variation of Friction Angle
(After Mayne et al. (2000))

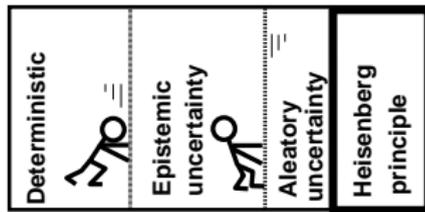
| Soil Property | Soil Type | PDF | Mean | COV (%) |
|--|---------------------|------|---------------------------|---------|
| Cone resistance | Sand Clay | LN | * | * |
| | Clay | N/LN | * | * |
| Undrained shear strength | Clay (triaxial) | LN | * | 5-20 |
| | Clay (index S_u) | LN | * | 10-35 |
| | Clayey silt | N | * | 5-15 |
| Ratio S_u/σ'_{vo} | Clay | N/LN | * | 5-15 |
| Plastic limit | Clay | N | 0.13-0.23 | 3-20 |
| Liquid limit | Clay | N | 0.30-0.80 | 3-20 |
| Submerged unit weight | All soils | N | 5-11 (kN/m ³) | 0-10 |
| Friction angle | Sand | N | * | 2-5 |
| Void ratio, porosity, initial void ratio | All soils | N | * | 7-30 |
| Over consolidation ratio | Clay | N/LN | * | 10-35 |

Typical COVs of Different Soil Properties (After Lacasse and Nadim 1996)

On Uncertainties

- ▶ Epistemic uncertainty - due to lack of knowledge

- ▶ Can be reduced by collecting more data
- ▶ Mathematical tools not well developed, trade-off with aleatory uncertainty



- ▶ Aleatory uncertainty - inherent variation of physical system
 - ▶ Can not be reduced
 - ▶ Has highly developed mathematical tools
- ▶ Ergodicity – exchange ensemble average for time average?
 - ▶ Applicable to soils, biomaterials, up for discussion for concrete, rock

Historical Overview

- ▶ Brownian motion, Langevin equation → PDF governed by simple diffusion Eq. (Einstein 1905)
- ▶ With external forces → Fokker-Planck-Kolmogorov (FPK) for the PDF (Kolmogorov 1941)
- ▶ Approach for random forcing → relationship between the autocorrelation function and spectral density function (Wiener 1930)
- ▶ Approach for random coefficient → Functional integration approach (Hopf 1952), Averaged equation approach (Bharrucha-Reid 1968), Monte Carlo method

Soil Uncertainties and Quantification

- ▶ Natural, spatial variability of soil deposit (Fenton 1999)
 - ▶ Function of soil formation process
- ▶ Testing (point-wise) error (Stokoe et al. 2004)
 - ▶ Imperfection of instruments
 - ▶ Error in methods to register quantities
- ▶ Transformation (point-wise) error (Phoon and Kulhawy 1999)
 - ▶ Correlation by empirical data fitting (e.g. CPT data → friction angle etc.)

Recent State-of-the-Art

- ▶ Governing equation
 - ▶ Dynamic problems $\rightarrow M\ddot{u} + C\dot{u} + Ku = \phi$
 - ▶ Static problems $\rightarrow Ku = \phi$
- ▶ Existing solution methods
 - ▶ **Random r.h.s** (external force random)
 - ▶ FPK equation approach
 - ▶ Use of fragility curves with deterministic FEM (DFEM)
 - ▶ **Random l.h.s** (material properties random)
 - ▶ Monte Carlo approach with DFEM \rightarrow CPU expensive
 - ▶ Perturbation method \rightarrow a linearized expansion! Error increases as a function of COV
 - ▶ Spectral method \rightarrow developed for elastic materials so far
- ▶ Newly developed: Stochastic Elastic–Plastic Finite Element Method

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Constitutive Problem Setup

- ▶ 3D incremental elasto–plasticity:

$$d\sigma_{ij}/dt = \left\{ D_{ijkl}^{el} - \frac{D_{ijmn}^{el} m_{mn} n_{pq} D_{pqkl}^{el}}{n_{rs} D_{rstu}^{el} m_{tu} - \xi_* r_*} \right\} d\epsilon_{kl}/dt$$

- ▶ Phase density ρ of $\sigma(x, t)$ varies in time according to a continuity Liouville equation (Kubo 1963)
- ▶ Continuity equation written in ensemble average form (eg. cumulant expansion method (Kavvas and Karakas 1996))
- ▶ van Kampen's lemma (van Kampen 1976) \rightarrow
 $\langle \rho(\sigma, t) \rangle = P(\sigma, t)$, ensemble average of phase density is the probability density

Eulerian–Lagrangian FPK Equation

$$\begin{aligned}
 \frac{\partial P(\sigma(x_t, t), t)}{\partial t} &= -\frac{\partial}{\partial \sigma} \left[\left\{ \left\langle \eta(\sigma(x_t, t), D^{el}(x_t), q(x_t), r(x_t), \epsilon(x_t, t)) \right\rangle \right. \right. \\
 + \int_0^t d\tau \text{Cov}_0 &\left[\frac{\partial \eta(\sigma(x_t, t), D^{el}(x_t), q(x_t), r(x_t), \epsilon(x_t, t))}{\partial \sigma}; \right. \\
 &\left. \left. \eta(\sigma(x_{t-\tau}, t-\tau), D^{el}(x_{t-\tau}), q(x_{t-\tau}), r(x_{t-\tau}), \epsilon(x_{t-\tau}, t-\tau)) \right\} P(\sigma(x_t, t), t) \right] \\
 + \frac{\partial^2}{\partial \sigma^2} &\left[\left\{ \int_0^t d\tau \text{Cov}_0 \left[\eta(\sigma(x_t, t), D^{el}(x_t), q(x_t), r(x_t), \epsilon(x_t, t)); \right. \right. \right. \\
 &\left. \left. \left. \eta(\sigma(x_{t-\tau}, t-\tau), D^{el}(x_{t-\tau}), q(x_{t-\tau}), r(x_{t-\tau}), \epsilon(x_{t-\tau}, t-\tau)) \right) \right] \right\} P(\sigma(x_t, t), t) \right]
 \end{aligned}$$

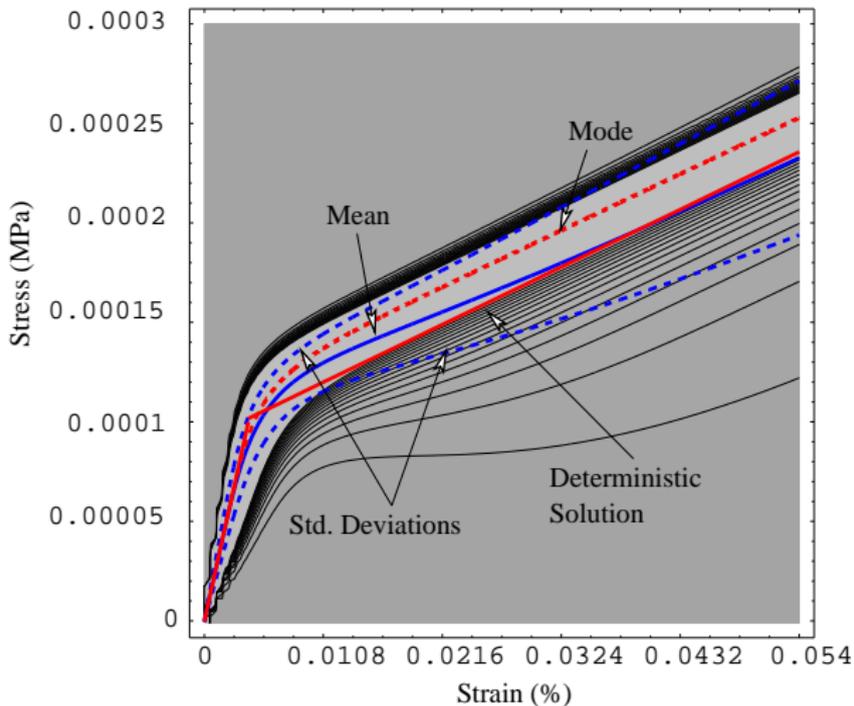
Euler–Lagrange FPK Equation

- ▶ Advection-diffusion equation

$$\frac{\partial P(\sigma, t)}{\partial t} = -\frac{\partial}{\partial \sigma} \left[N_{(1)} P(\sigma, t) - \frac{\partial}{\partial \sigma} \{ N_{(2)} P(\sigma, t) \} \right]$$

- ▶ Complete probabilistic description of response
- ▶ Solution PDF is second-order exact to covariance of time (exact mean and variance)
- ▶ It is deterministic equation in probability density space
- ▶ It is linear PDE in probability density space → Simplifies the numerical solution process
- ▶ Template FPK diffusion–advection equation is applicable to any material model → only the coefficients $N_{(1)}$ and $N_{(2)}$ are different for different material models

Transformation of a Bi-Linear (von Mises) Response



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Stochastic Finite Element Formulation

- ▶ Governing equations:

$$A\sigma = \phi(t); \quad Bu = \epsilon; \quad \sigma = D\epsilon$$

- ▶ **Spatial** and **stochastic** discretization
 - ▶ Deterministic spatial differential operators (A & B) → Regular shape function method with Galerkin scheme
 - ▶ Input random field material properties (D) → Karhunen–Loève (KL) expansion, optimal expansion, error minimizing property
 - ▶ Unknown solution random field (u) → Polynomial Chaos (PC) expansion

Spectral Stochastic Elastic–Plastic FEM

- ▶ Minimizing norm of error of finite representation using Galerkin technique (Ghanem and Spanos 2003):

$$\sum_{n=1}^N K_{mn}^{ep} d_{ni} + \sum_{n=1}^N \sum_{j=0}^P d_{nj} \sum_{k=1}^M C_{ijk} K_{mnk}'^{ep} = \langle F_m \psi_i[\{\{\xi_r\}\}] \rangle$$

$$K_{mn}^{ep} = \int_D B_n D^{ep} B_m dV$$

$$C_{ijk} = \langle \xi_k(\theta) \psi_i[\{\{\xi_r\}\}] \psi_j[\{\{\xi_r\}\}] \rangle$$

$$K_{mnk}'^{ep} = \int_{D_r} B_n \sqrt{\lambda_k} h_k B_m dV$$

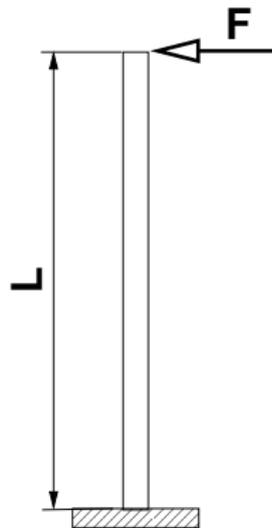
$$F_m = \int_D \phi N_m dV$$

Inside SEPFEM

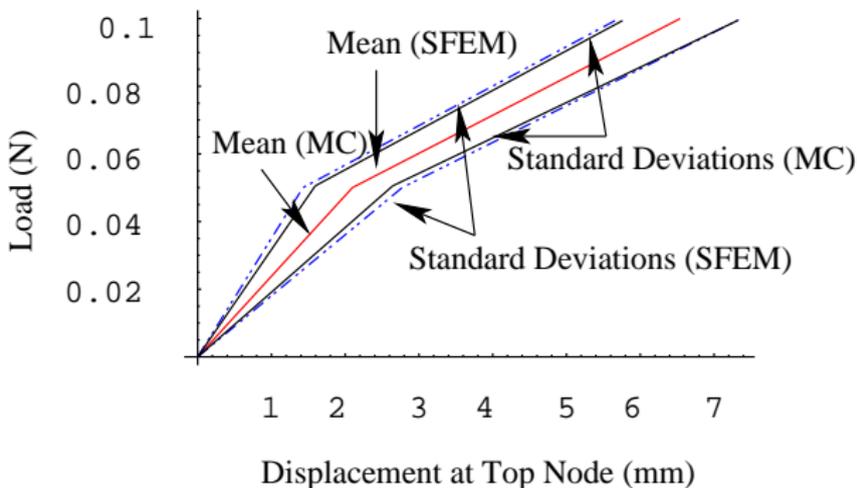
- ▶ Explicit stochastic elastic–plastic finite element computations
- ▶ FPK probabilistic constitutive integration at Gauss integration points
- ▶ Increase in (stochastic) dimensions (KL and PC) of the problem (parallelism)
- ▶ Development of the probabilistic elastic–plastic stiffness tensor

1–D Static Pushover Test Example

- ▶ Elastic–plastic material model, von Mises, linear hardening,
 $\langle G \rangle = 2.5 \text{ kPa}$,
 $\text{Var}[G] = 0.15 \text{ kPa}^2$,
correlation length for $G = 0.3 \text{ m}$,
 $C_u = 5 \text{ kPa}$,
 $C'_u = 2 \text{ kPa}$.



SEPFEM verification



Mean and standard deviations of displacement at the top node, von Mises elastic-plastic linear hardening material model, KL-dimension=2, order of PC=2.

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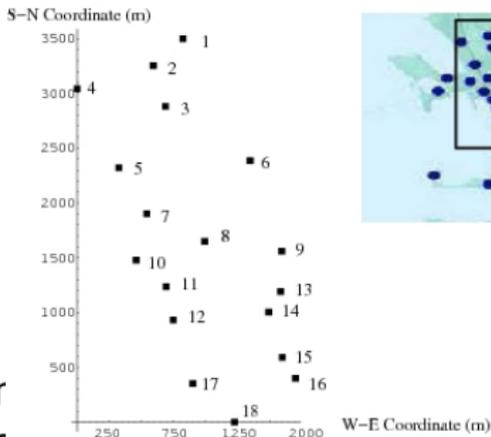
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Seismic Wave Propagation Through Random Soil

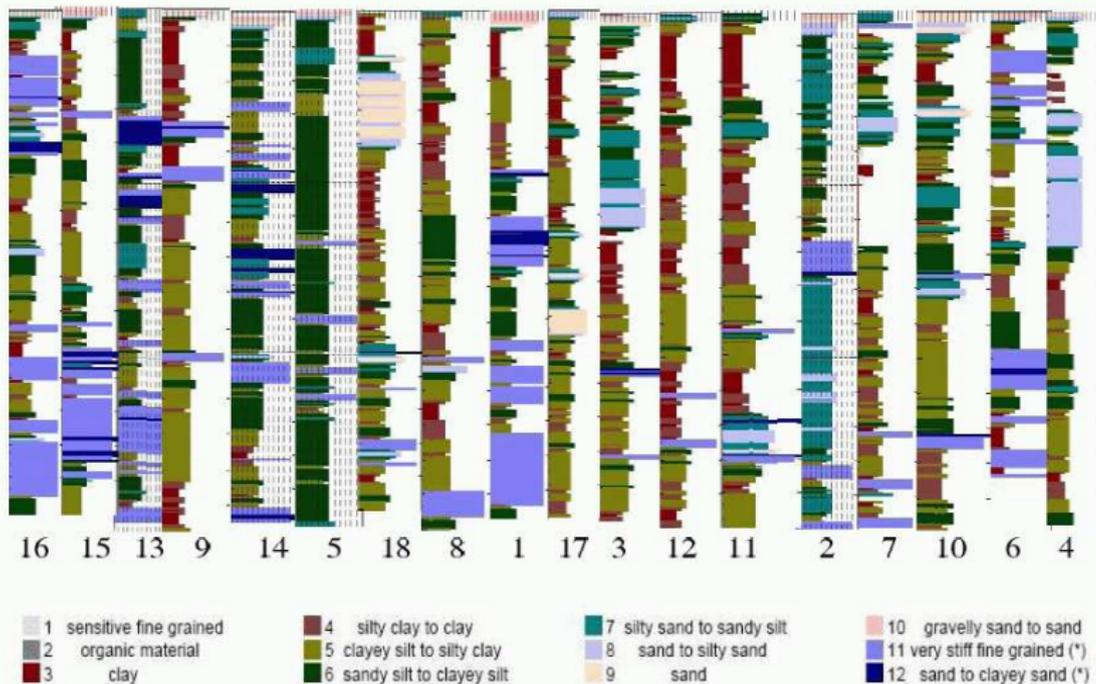
Soil is 12.5 m deep 1-D soil column with random von Mises material:

- ▶ Shear modulus:
 - $\langle G \rangle = 11.57 \text{ MPa}$;
 - $\text{Var}[G] = 142.32 \text{ MPa}^2$;
 - Cor. Length $[G] = 0.61 \text{ m}$
- ▶ Shear strength:
 - $\langle q_T \rangle = 4.99 \text{ MPa}$;
 - $\text{Var}[q_T] = 25.67 \text{ MPa}^2$;
 - Cor. Length $[q_T] = 0.61 \text{ r}$
 - Testing Error = 2.78 MPa



Seismic Wave Propagation Through Uncertain Soils

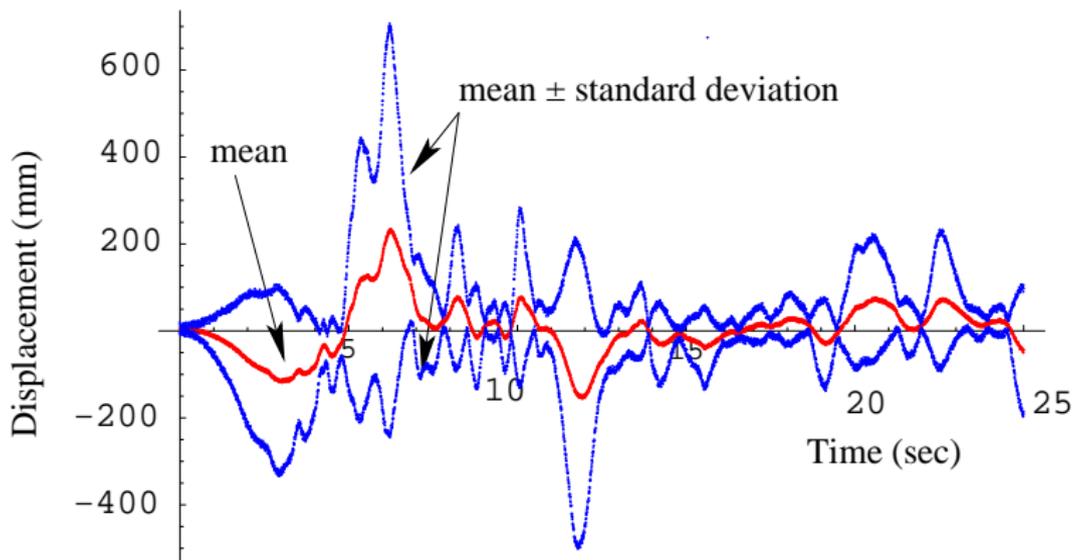
"Uniform" Soil Site

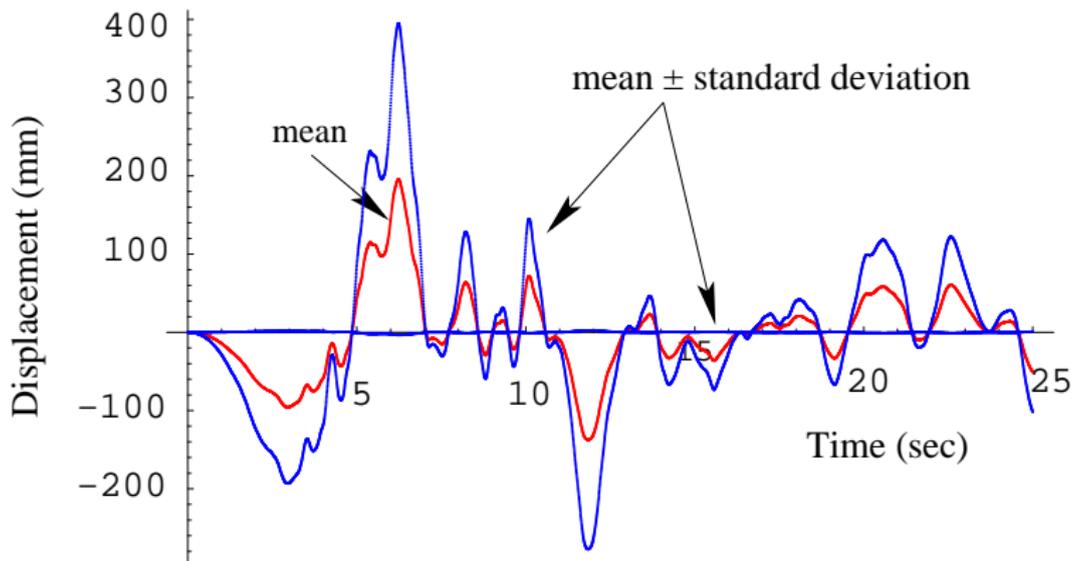


Three Approaches to Modeling

- ▶ Do nothing about site characterization (rely on experience): conservative **guess** of soil data, $COV = 225\%$, correlation length = 12m.
- ▶ Do better than standard site characterization: $COV = 103\%$, correlation length = 0.61m)
- ▶ Improve site (material) characterization if probabilities of exceedance are unacceptable!

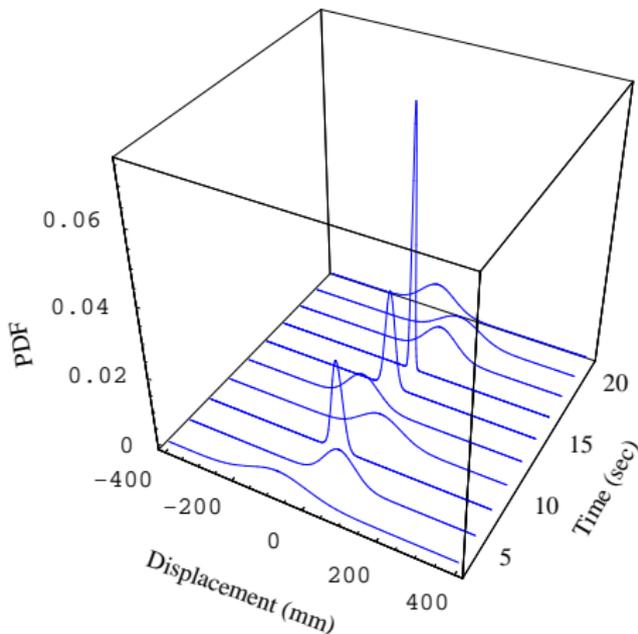
Evolution of Mean \pm SD for Guess Case



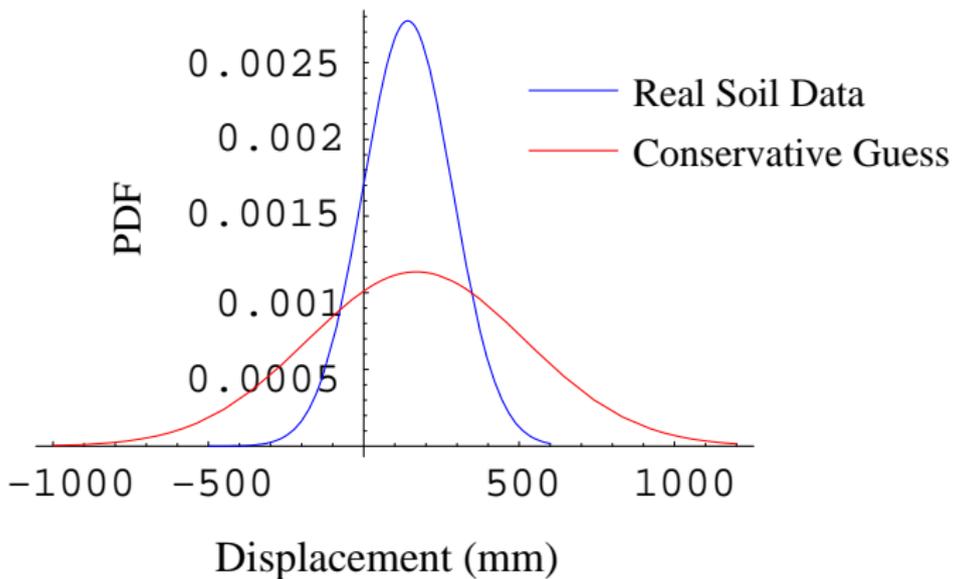
Evolution of Mean \pm SD for Real Data Case

Full PDFs for Real Data Case

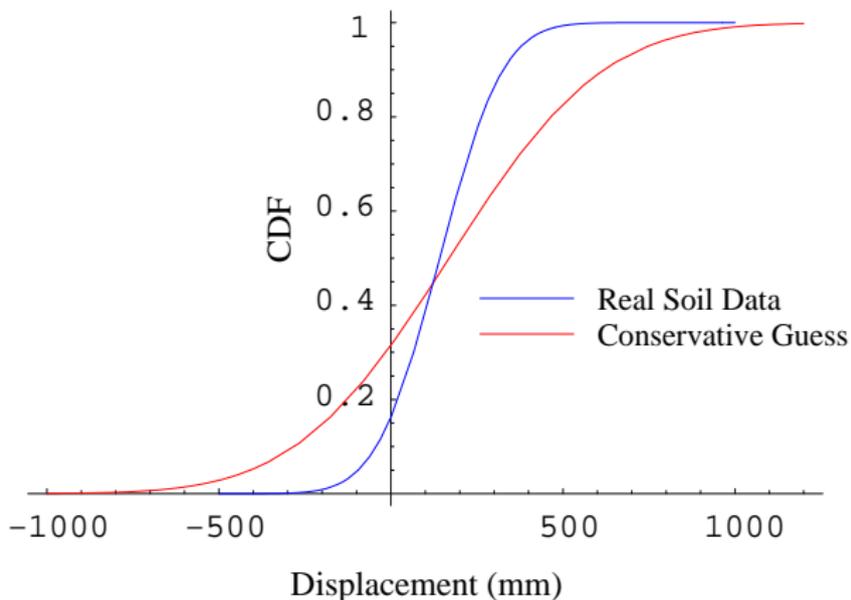
- ▶ PDF at the finite element nodes can be obtained using, e.g., Edgeworth expansion (Ghanem and Spanos 2003)
- ▶ Numerous applications, especially where extreme statistics are critical



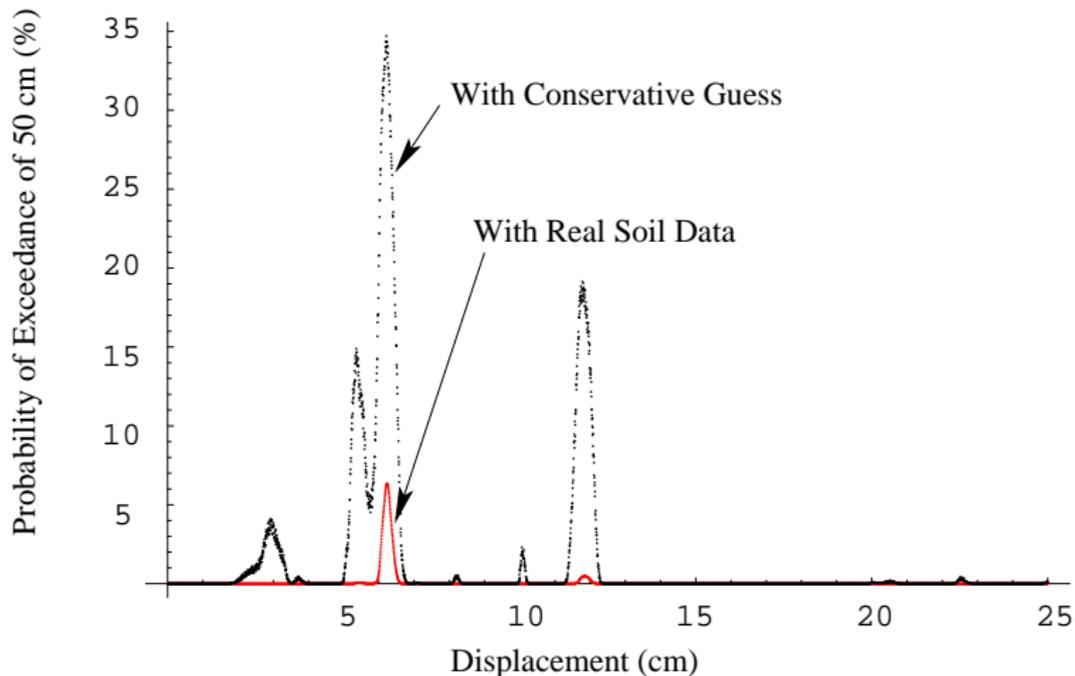
Example: PDF at 6 s



Example: CDF at 6 s



Probability of Exceedance of 50cm



Summary

- ▶ Behavior of materials is probably probabilistic, and one probably has to deal with it (in a probabilistic way)!
- ▶ Probabilistic Elasto–Plasticity and Stochastic Elastic–Plastic Finite Element Methodology has been developed and is being refined
- ▶ Human nature: how much do you want to know about potential problem?