

# Nonlinear Soil Modeling for Seismic NPP Applications

Boris Jeremić and Federico Pisanò

University of California, Davis  
Lawrence Berkeley National Laboratory, Berkeley

LBLN Seminar, December 2012

# Outline

Introduction

Elastic-Plastic Models

Summary

# Outline

Introduction

Elastic-Plastic Models

Summary

# The Problem

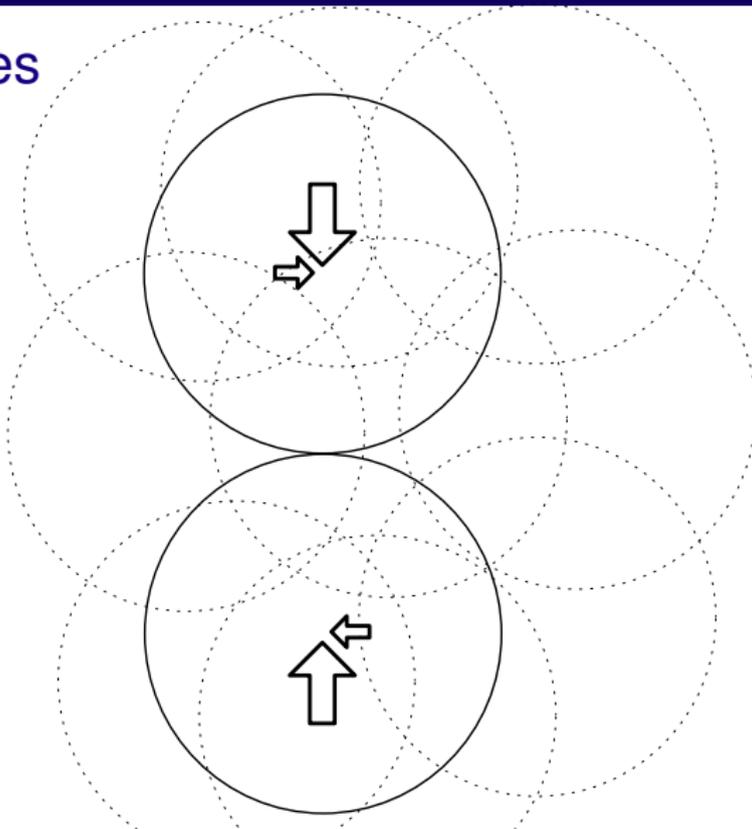
- ▶ Seismic response of Nuclear Power Plants
- ▶ Soil modeling in particular
- ▶ Linear elastic
- ▶ Equivalent Linear Elastic (current state of practice/art)
- ▶ 3D elastic-plastic modeling
- ▶ Combine frictional (elastic-plastic, displacement proportional) and viscous (velocity proportional) energy dissipation in one model.



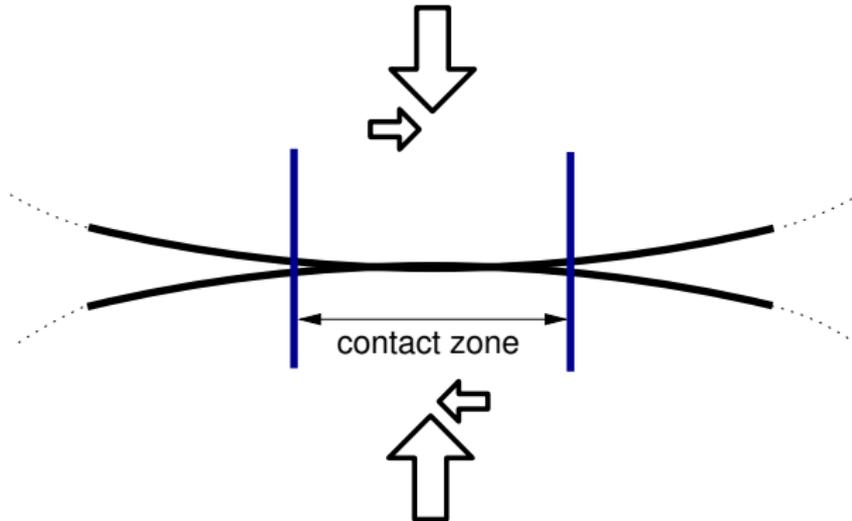
# Granular Materials

- ▶ Pressure sensitive materials (particles)
- ▶ Usually assumed to be linear elastic (at least in the NPP field (?!))
- ▶ Can be (rigorously) shown that as they can never be linear elastic (with normal and/or shear contact forces.
- ▶ R. D. Mindlin and H. Deresiewicz. Elastic spheres in contact under varying oblique forces. *ASME Journal of Applied Mechanics*, 53(APM-14):327-344, September 1953.
- ▶ Izhak Etsion. Revisiting the Cattaneo-Mindlin concept of interfacial slip in tangentially loaded compliant bodies. *Journal of Tribology*, 132(2):020801, 2010.

# Two Spheres

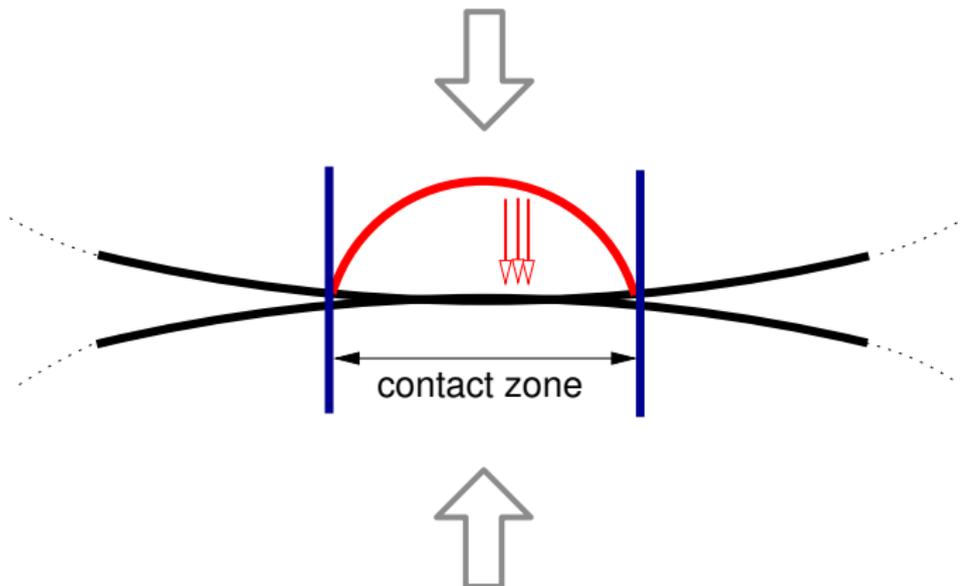


# Contact Zone



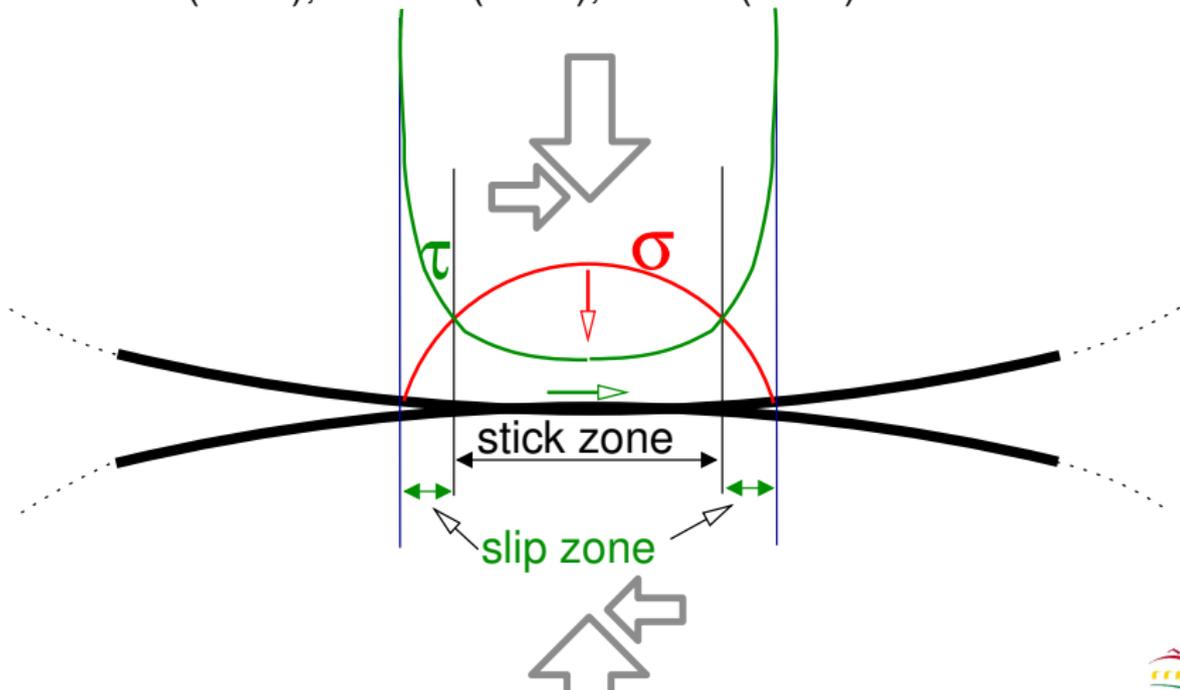
# Normal Stresses

## Hertz (1882)



# Normal and Shear Stresses

Cattaneo (1938), Mindlin (1949), Etsion (2010)



# Granular Materials (Summary)

- ▶ Particulate materials are never linear elastic

# Outline

Introduction

**Elastic-Plastic Models**

Summary

# von Mises perfectly plastic model

- ▶  $f = \sqrt{\frac{3}{2} s_{ij} s_{ij}} - \sigma_0 = 0$
- ▶ undrained shear strength  $s_u$  ( $s_u = \sigma_0 / \sqrt{3}$ )

## Drucker-Prager kinematic hardening model

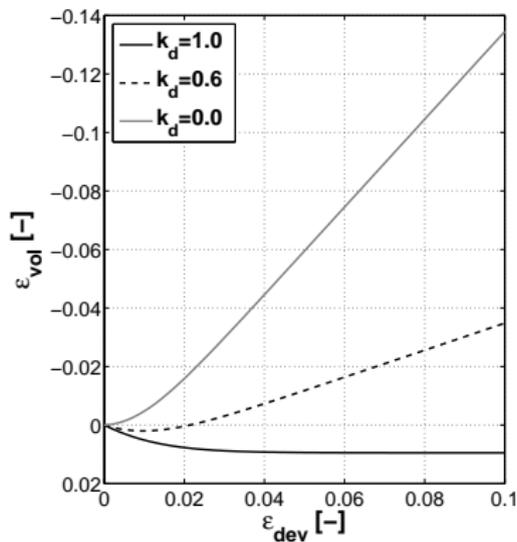
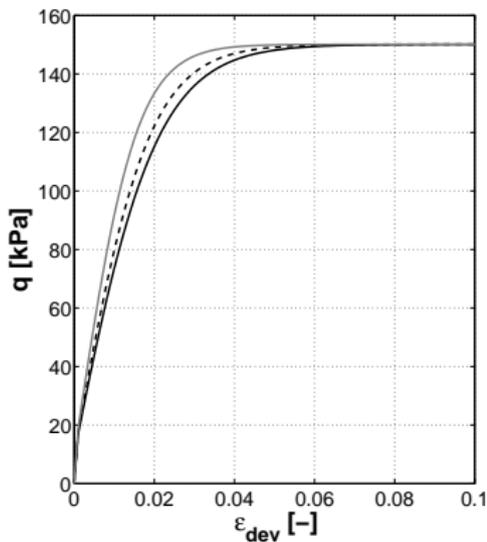
$$\triangleright f = \sqrt{(s_{ij} - p\alpha_{ij})(s_{ij} - p\alpha_{ij})} - \sqrt{\frac{2}{3}}kp = 0$$

$$\triangleright \epsilon_{ij}^p = \dot{\lambda}m_{ij}, m_{ij} = \left(\frac{\partial f}{\partial \sigma_{ij}}\right)^{dev} - \frac{1}{3}D\delta_{ij},$$

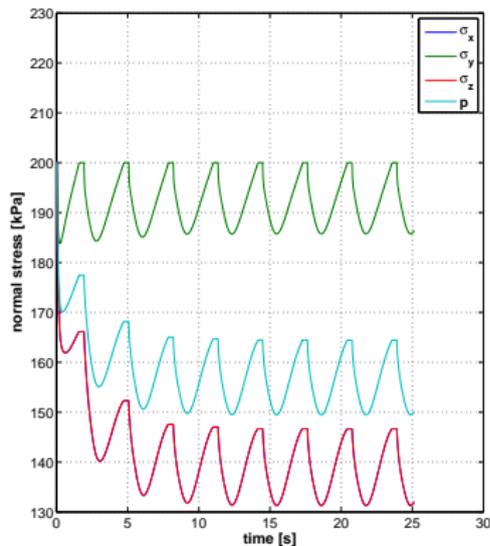
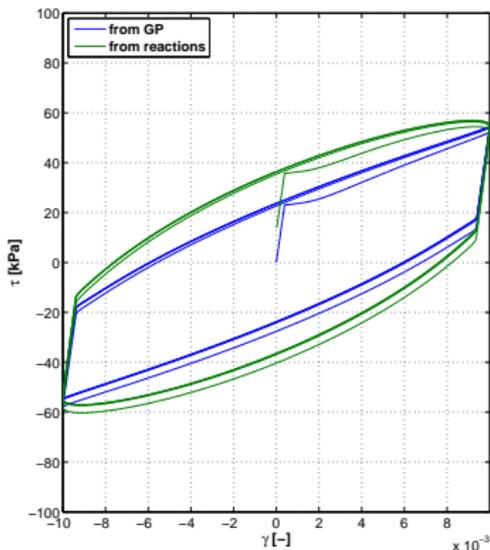
dilatancy coefficient  $D = \xi \left( \sqrt{\frac{2}{3}}k_d - \sqrt{r_{mn}r_{mn}} \right)$

$$\triangleright \dot{\alpha}_{ij} = \frac{2}{3}h_a \left(\epsilon_{ij}^p\right)^{dev} - c_r\alpha_{ij}\sqrt{\frac{2}{3}} \left(\epsilon_{rs}^p\right)^{dev} \left(\epsilon_{rs}^p\right)^{dev}$$

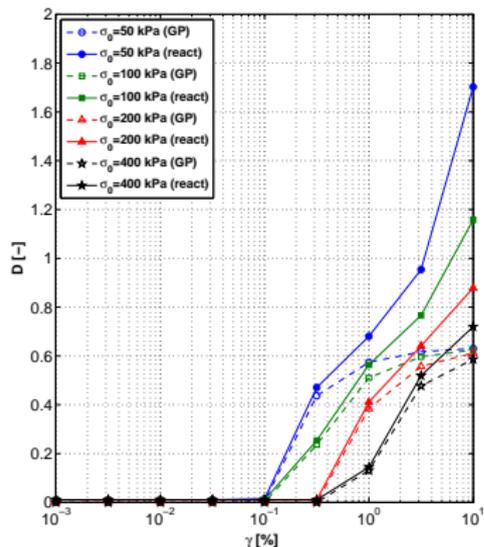
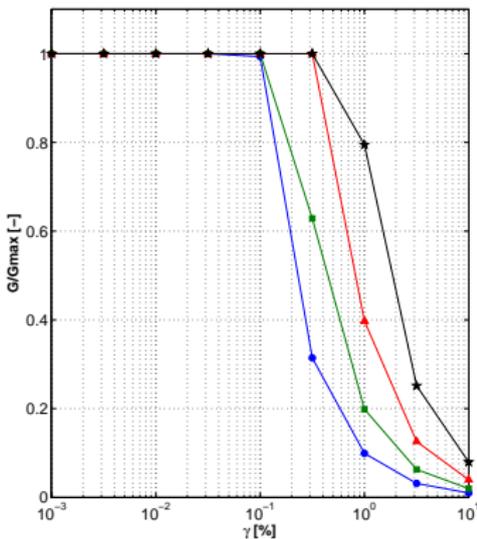
# Drucker-Prager kinematic hardening model



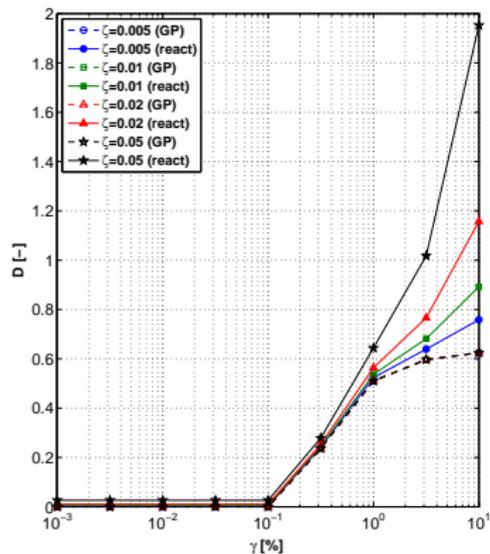
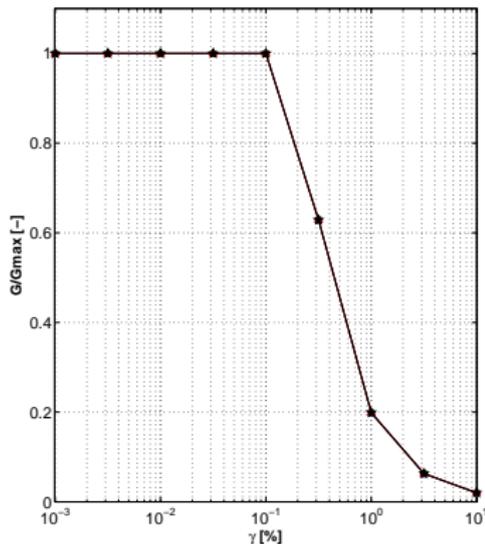
# Drucker-Prager Kinematic Hardening Model with Viscosity



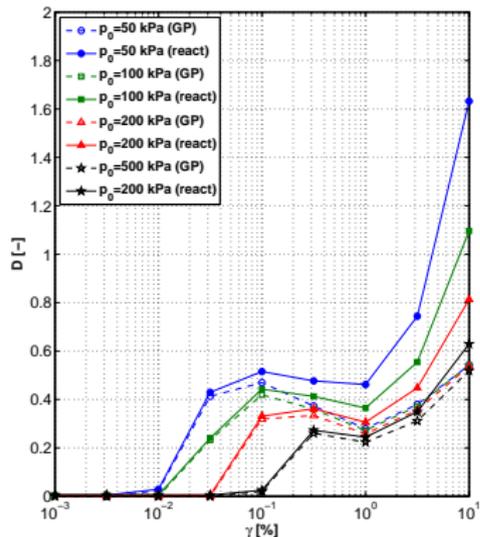
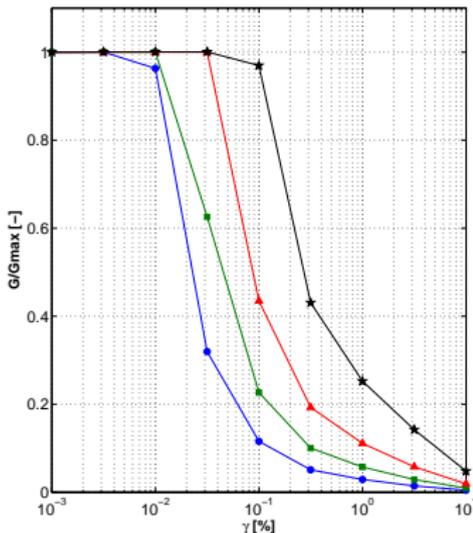
## DK - Variation in Yield Stress



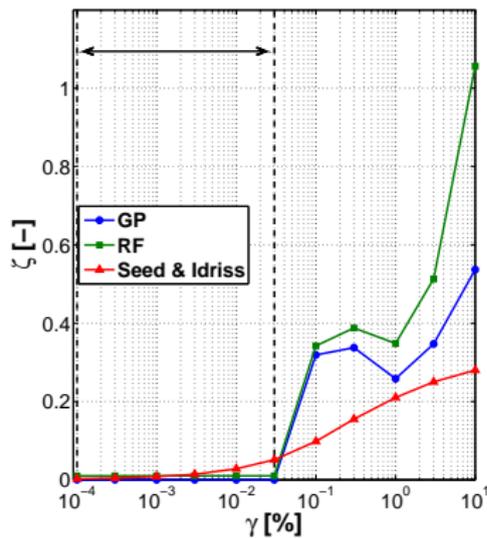
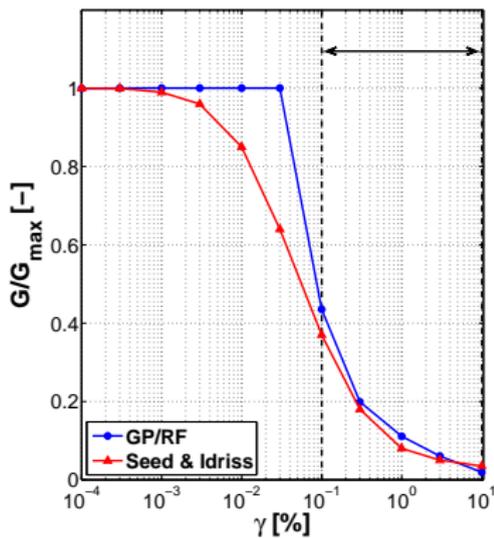
## DK - Variation in Damping Coefficient



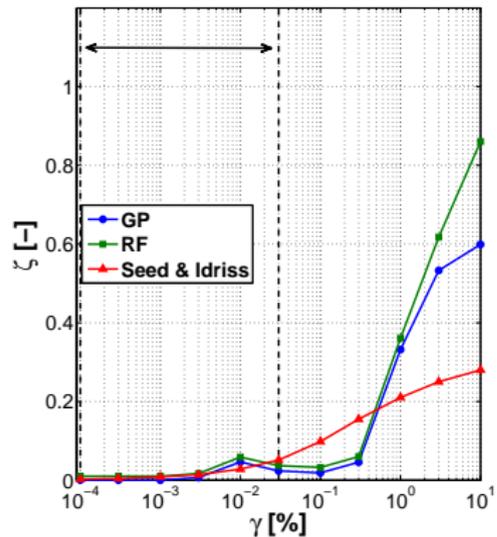
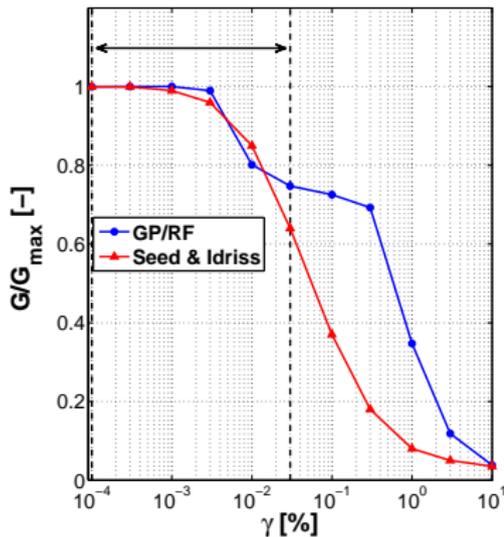
## DK - Variation in Initial Confinement



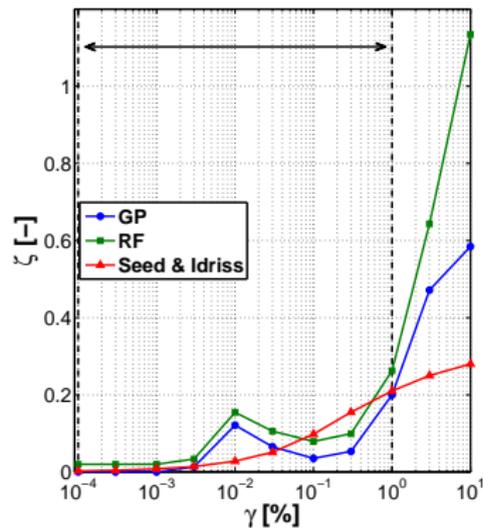
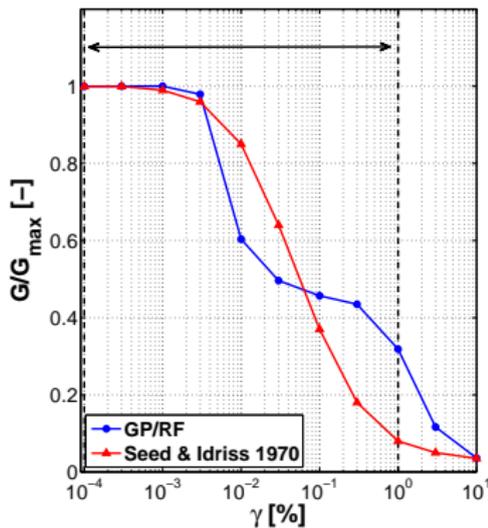
# Comparison with $G/G_{max}$ and Damping Curves



# Comparison with $G/G_{max}$ and Damping Curves



# Comparison with $G/G_{max}$ and Damping Curves



# PJ Model: Assumptions

- ▶ Split stress into frictional and viscous components

$$\sigma_{ij} = \sigma_{ij}^f + \sigma_{ij}^v$$

- ▶ Remove the elastic region (limit analysis)
- ▶ Rotating kinematic hardening

# PJ Model: Elasticity

$$d\sigma_{ij} = D_{ijhk}^e (d\epsilon_{hk} - d\epsilon_{hk}^p)$$

$$ds_{ij} = 2G_{max} (de_{hk} - de_{hk}^p)$$

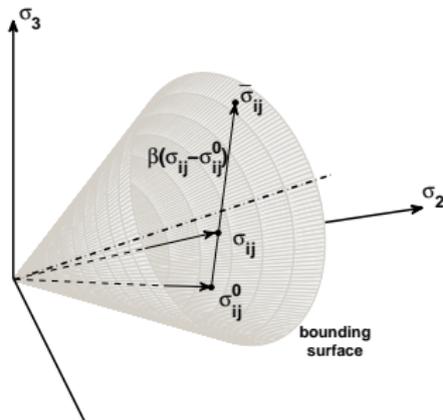
$$dp = -K (d\epsilon_{vol} - d\epsilon_{vol}^p)$$

where  $p = -\sigma_{kk}/3$ ,  $\epsilon_{vol} = \epsilon_{kk}$ ,  $s_{ij} = \sigma_{ij}^{dev}$ ,  $e_{ij} = \epsilon_{ij}^{dev}$ ,  
 $G_{max} = E/2(1 + \nu)$  and  $K = E/3(1 - 2\nu)$

# PJ Model: DP Yield and Bounding Surface

$$f_y = \frac{3}{2} (s_{ij} - p\alpha_{ij}) (s_{ij} - p\alpha_{ij}) - k^2 p^2 = 0$$

$$f_B = \frac{3}{2} s_{ij} s_{ij} - M^2 p^2 = 0$$



## PJ Model: Plastic Flow and Translation Rule

Borrowed from Manzari and Dafalias (1997)

$$d\epsilon_{hk}^p = d\lambda \left( n_{ij}^{dev} - \frac{1}{3} D \delta_{ij} \right)$$

$$D = \xi \left( \alpha_{ij}^d - \alpha_{ij} \right) n_{ij}^{dev} = \xi \left( \sqrt{\frac{2}{3}} k_d n_{ij}^{dev} - \alpha_{ij} \right) n_{ij}^{dev}$$

$$d\alpha_{ij} = \|d\alpha_{ij}\| n_{ij}^{dev}$$

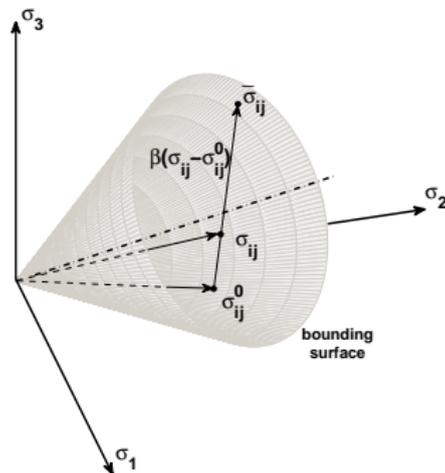
# PJ Model: Vanishing Elastic Region

$$\lim_{k \rightarrow 0} f_y = 0 \Rightarrow \lim_{k \rightarrow 0} s_{ij} = p\alpha_{ij} \Rightarrow ds_{ij} = d\alpha_{ij}p + \alpha_{ij}dp$$

$$n_{ij}^{dev} = \frac{ds_{ij} - \alpha_{ij}dp}{\|ds_{ij} - \alpha_{ij}dp\|}$$

$$\|d\alpha_{ij}\| = \frac{1}{pN^{dev}} \frac{\partial f}{\partial \sigma_{ij}} d\sigma_{ij}$$

$$\|d\alpha_{ij}\| = \sqrt{\frac{2}{3}} \frac{dq}{p}$$



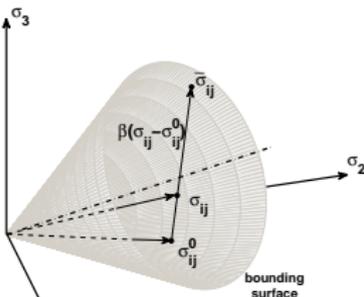
# PJ Model: Hardening Modulus and Plastic Multiplier

$$\|d\alpha_{ij}\| = \frac{2}{3} \frac{H d\lambda}{p}$$

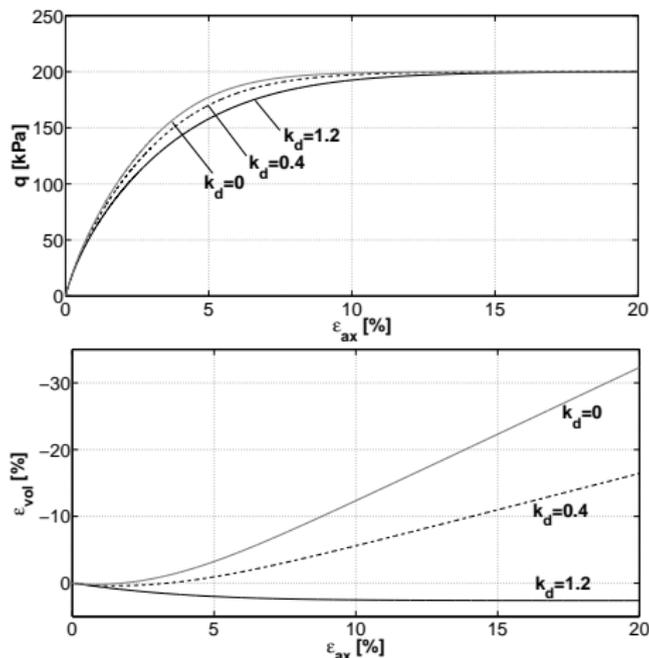
$$d\lambda = \frac{2G_{max} \|de_{ij}\| + Kd\epsilon_{vol}\alpha_{ij}n_{ij}^{dev}}{2G + \frac{2}{3}H - KD\alpha_{ij}n_{ij}^{dev}}$$

# PJ Model: Stress Projection, Hardening and Unloading

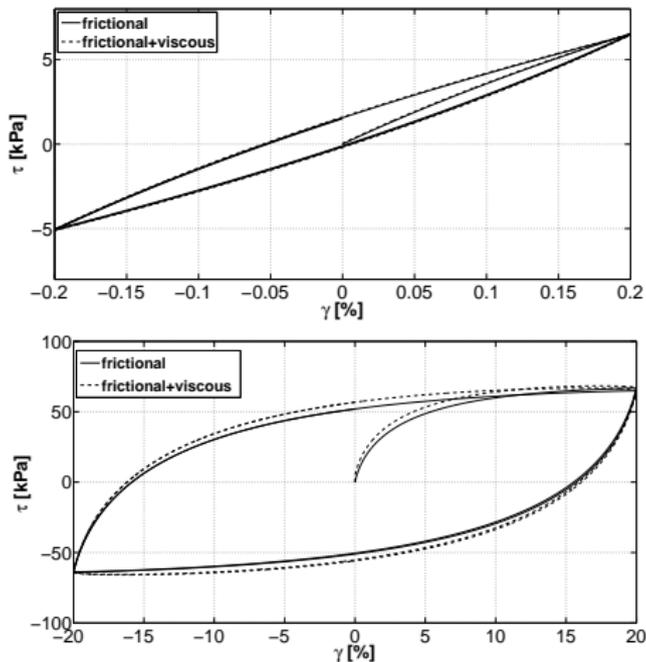
$$d\beta = - (1 + \beta) \frac{\bar{s}_{ij} ds_{ij} - \frac{2}{3} M^2 \bar{p} dp}{\bar{s}_{ij} (s_{ij} - s_{ij}^0) - \frac{2}{3} M^2 \bar{p} (p - p^0)} > 0$$



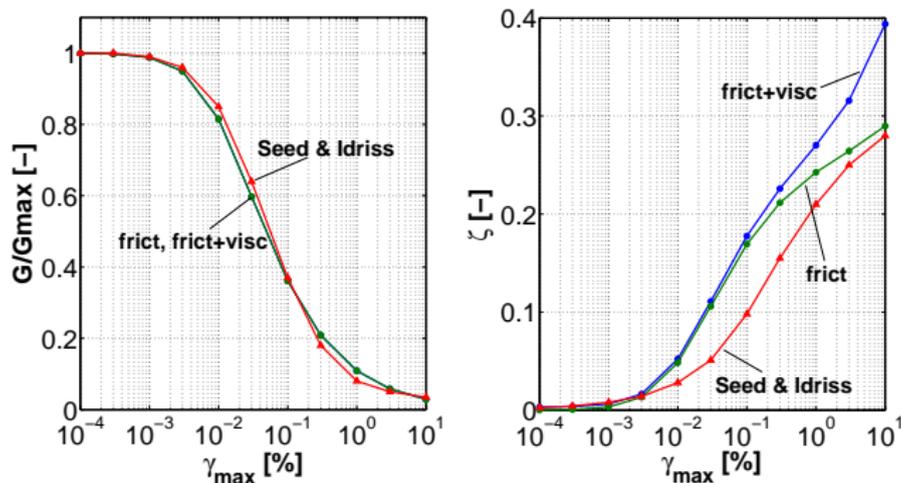
# PJ Model: Triaxial Response



# PJ Model: Pure Shear Cyclic

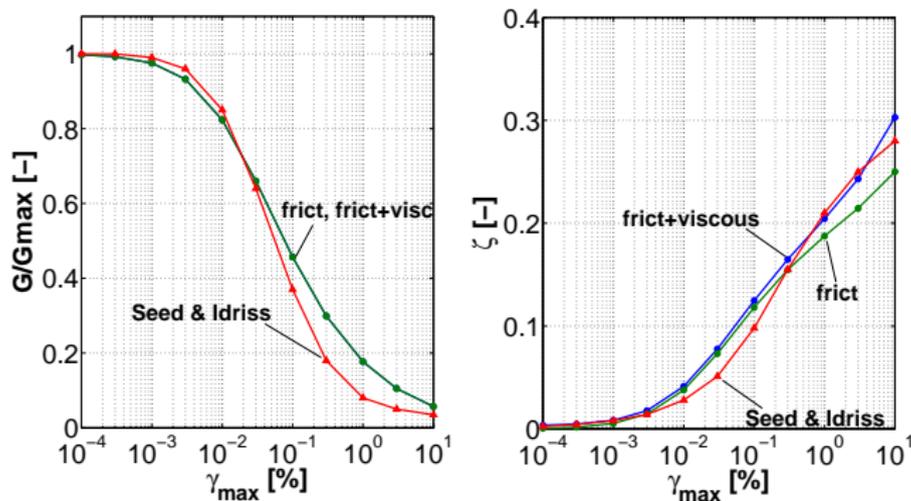


# PJ Model: Calibration for $G/G_{max}$ and Damping



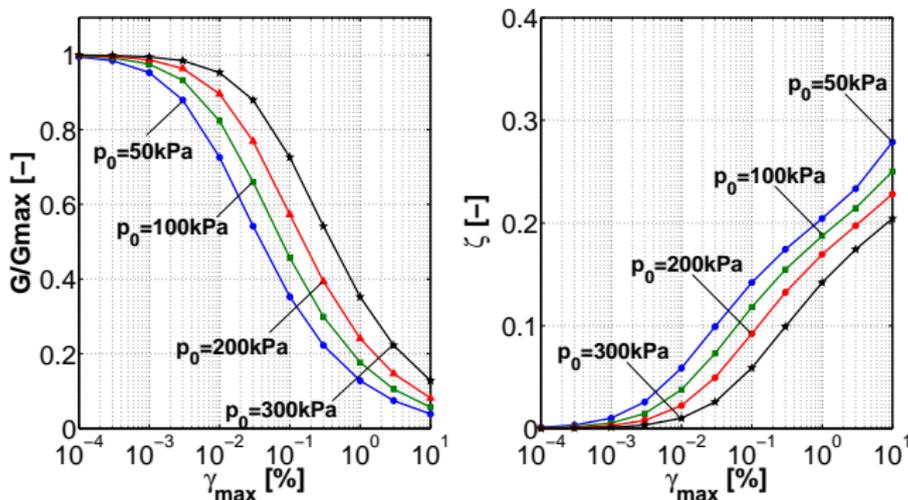
**Figure:** Comparison between experimental and simulated  $G/G_{max}$  and damping curves ( $p_0=100$  kPa,  $T=2\pi$  s,  $\zeta = 0.003$ ,  $G_{max} = 4$  MPa,  $\nu=0.25$ ,  $M=1.2$ ,  $k_d=\xi=0$ ,  $h=G/(112p_0)$ ,  $m=1.38$ )

# PJ Model: Calibration for $G/G_{max}$ and Damping



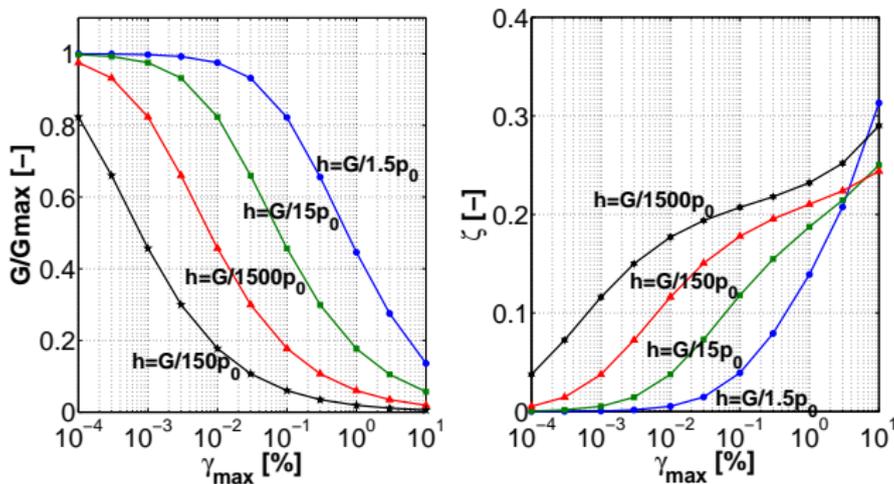
**Figure:** Comparison between experimental and simulated  $G/G_{max}$  and damping curves ( $p_0=100$  kPa,  $T=2\pi$  s,  $\zeta = 0.003$ ,  $G_{max} = 4$  MPa,  $\nu=0.25$ ,  $M=1.2$ ,  $k_d=\xi=0$ ,  $h=G_{max}/(15p_0)$ ,  $m=1$ )

# PJ Model: Variation in Confining Pressure



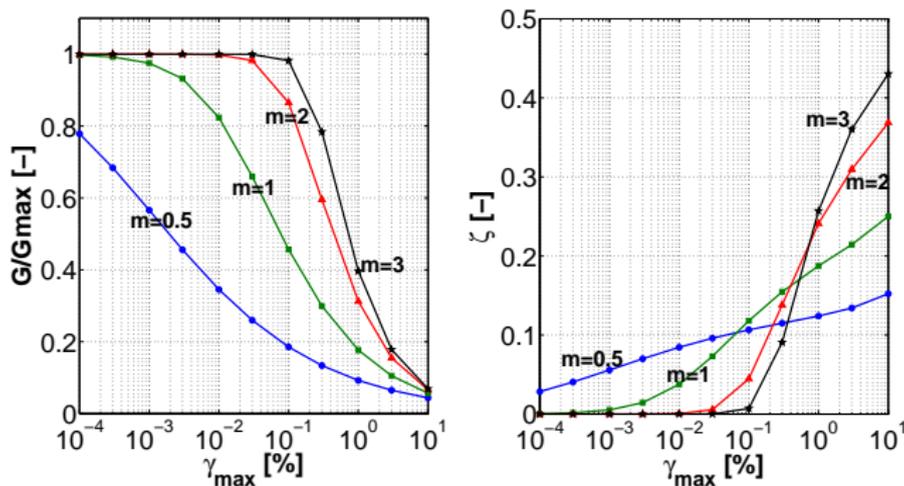
**Figure:** Simulated  $G/G_{max}$  and damping curves at varying confining pressure ( $T=2\pi$  s,  $G_{max} = 4$  MPa,  $\nu=0.25$ ,  $M=1.2$ ,  $k_d=\xi=0$ ,  $h=G/(15p_0)$ ,  $m=1$ )

# PJ Model: Variation in Hardening Parameter $h$



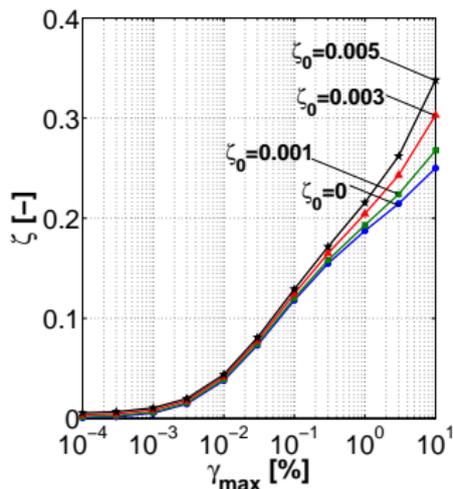
**Figure:** Simulated  $G/G_{max}$  and damping curves at varying  $h$  ( $p_0=100$  kPa,  $T=2\pi$  s,  $G_{max} = 4$  MPa,  $\nu=0.25$ ,  $M=1.2$ ,  $k_d=\xi=0$ ,  $m=1$ )

# PJ Model: Variation in Hardening Parameter $m$



**Figure:** Simulated  $G/G_{max}$  and damping curves at varying  $m$  ( $p_0=100$  kPa,  $T=2\pi$  s,  $G_{max} = 4$  MPa,  $\nu=0.25$ ,  $M=1.2$ ,  $k_d=\xi=0$ ,  $h=G_{max}/(15p_0)$ )

# PJ Model: Variation in Viscous Damping



**Figure:** Damping curves simulated at varying  $\zeta_0$  ( $p_0=100$  kPa,  $T=2\pi$  s,  $G_{max} = 4$  MPa,  $\nu=0.25$ ,  $M=1.2$ ,  $k_d=\xi=0$ ,  $h=G_{max}/(15p_0)$ ,  $m=1$ )

# Outline

Introduction

Elastic-Plastic Models

Summary

## Summary

- ▶ Frictional and Viscous energy dissipation for granular materials
- ▶ Classical elastic-plastic models with addition of viscous damping
- ▶ Vanishing elastic region elastic-plastic material model
- ▶ Important for professional practice since  $G/G_{max}$  and damping curves (all just in 1D !) is what is available, and this model calibrates well, and is full 3D model.